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A New Strategy using High Density PWM Converter in Single Phase to Three Phase Drive System for WECS Application

Mrs. J. Steffy

Assistant Professor, Electrical and Electronics Engineering, Apollo Engineering College, Chennai

Abstract: The proposed system permits to reduce the rectifiers switching currents, the harmonics distortion at the input converter side, and improvements on the fault tolerance characteristics. Single phase to three phase drive system composed of High density PWM rectifier, a three phase inverter and PMSG. The feed-forward method can help the auxiliary active energy storage circuit working as a parallel active power filter for filtering out the low frequency ripple current from the H-bridge rectifier. The total energy loss of the proposed system may be lower than that of a conventional one. Suitable control strategy including the pulse width modulation technique is developed.

Index Terms: Ac-dc-ac power converter, drive system, parallel converter.

I. INTRODUCTION

High density PWM converter is used to improve the power capability, reliability and efficiency. This technique can be employed to improve the performance of active power filter, un interruptible power supplies, fault tolerance of induction motor and three phase drives. Usually the operation of converters in parallel requires a transformer for isolation. The weight, size, and cost associated with the transformer is high hence makes the system bulky. In this proposed parallel converters isolation transformers are not used so that this system is highly reliable.

Single phase to three phase drive system composed of single phase High Density rectifiers and a three phase inverter. This parallel converter topology permits to reduce the rectifier switch current, the total harmonic distortion (THD) of the grid current with same switching frequency with same THD of the grid current and to increase the fault tolerance characteristics. The control strategy employed for this single phase to three phase conversion is PID controller and harmonics can be reduced using PWM techniques.







Fig.2 Proposed single phase to three phase drive system



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II.AUXILLARY CIRCUIT

For a practical implementation, it is not easy to determine the auxiliary capacitor current reference A more straightforward, but similar current filter method is used. The compensation current is used to regulate the low frequency ripple current. the triangular shaded area is the current waveform of the compensation current.



Figure 3.Auxillary circuit working as parallel active ripple current filter

Using the previous method, the average compensation current within one switching period should be equal to the low frequency ripple current.

III.PWM STRATEGY

The control of output voltage control involves the variation of dc input voltage; regulate the variation of inverters and to satisfy the constant volts and frequency control requirements. The most efficient method of controlling inverter output is pulse width modulation technique (PWM). The change of position of voltage pulse leads also to change in the distribution of the zero instantaneous voltage. The parameter ' μ ' influence the harmonic distortion of the voltages generated by the rectifiers. When $\mu = 0$ or $\mu = 1$ the zero voltages are placed at the beginning or at the end of the switching period. When $\mu = 0.5$ they are distributed equally at the beginning and at the end of the half period. It is similar to distribution of the zero-voltage vector in three phase inverter.

IV.CONTROL STRATEGY



Fig 4.control block diagram

Control of rectifier has some objectives like to control the dc-link voltage and to make the power factor equals to one. The circulating current i_0 in the rectifier needs to be controlled. The dc link voltage v_c is adjusted to its reference value v_c^* using the PID controller R_c . To control power factor and harmonics in the grid side, the instantaneous reference current i_g^* must be synchronized with voltage e_g for the voltage oriented control (VOC) for the three phase system. The control of rectifiers can be implemented by the controller R_a and R_b . The control system is composed of PWM commanded and a torque/flux strategy.

V. HARMONIC DISTORTION

The harmonic distortion of the converter voltages has been evaluated by using the weighted THD (WTHD). WTHD can be calculated by using the fallowing formula,

WTHD (p) = $100/a_1$ Where $\sqrt{\sum_{i=2}^{p} \zeta}$

$$\sqrt{\sum_{i=2}^{p} (ai / i)2}$$

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 a_1 is the amplitude of the fundamental voltage, a_i is the amplitude of i^{th} harmonic and p is the number of harmonics taken into consideration.

The resultant voltage v_{ab} is used to regulate the harmonic distortion of the utility grid. The WTHD of the proposed topology in double-carrier with $\mu=0$ or $\mu=1$ is close to 63% of that conventional bridge rectifier with $\mu=0.5$ and the switching frequency can be reduced upto 60%.



Figure 5. Harmonic distortion curve

For the double-carrier the voltage v_{ab} has smaller amplitude and better distribution along the half switching period than that of single carrier. the optimal rectifier operation is obtained with double carrier making $\mu = 0$ or $\mu = 1$ with the reduced losses and increased efficiency

VI.INPUT INDUCTORS

The curve indicates total harmonic distortion for different values of l_n . for $l_n > 0.4$ ($l_g' > 0.4l_g$) the THD of the grid current of the proposed topology is smaller than that of the conventional topology. The harmonic distortion of the rectifier currents is higher than that of the grid current i_g . The adequate choice of the PWM strategy permits to operate with minimum harmonic distortion.



VII.FAULT COMPENSATION

The fault compensation is achieved by reconfiguring the power converter topology with help of isolating devices and connecting devices. Fault identification system (FIS) detects and locates the faulty switches, defining the leg to be isolated. If a fault in any switch of rectifier A has been detected by the control system, the whole rectifier needs to be isolated. This isolation procedure depends on the kind of fault detected. If an open-circuits failure is detected, the control system will open all switches of the rectifier A, and in this case, the fuses will open, and consequently, the rectifier will be isolated.



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Figure 7.Fault compensation block

VIII.SIMULATION RESULTS



Fig 8.High density single phase rectifier controller block







Fig 10.PWM generation block



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Fig 14. μ and dc voltage curve



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TABLE I Normalized THD of the dc link current of the proposed converter

Topology (PWM)		THD _p / THD _c
Proposed	(single μ =0.5)	0.994
Proposed	(double μ =0.5)	1.002
Proposed	double µ=0)	0.717

TABLE II Efficiency of the proposed system

(np/nc-1)					
Frequency/inductor	S-Ca µ=0.5	D-Ca µ=0.5	D-Ca µ=0		
10KHZ/(Lg'=Lg)	-1.60%	-1.47%	-0.41%		
10KHZ/(Lg'=Lg/2)	3.12%	3.25%	4.36%		
5KHZ/(Lg'=Lg)	-0.74%	-0.27%	1.72%		

IX.LOSSES AND EFFICIENCY

When the rectifier operates with a switching frequency equal to 5 KHZ, the conduction and switching losses of proposed topology were 70% and 105%, respectively, of the corresponding losses of the conventional topology. The efficiency of the topologies operating with a switching frequency equal to 10 KHZ and 5KHZ was evaluated experimentally. In the other cases, the proposed configuration with double-carrier and μ =0 presents higher efficiency than the conventional one.

X.COSTS AND APPLICATIONS OF CONFIGURATION

The initial investment of the proposed system is higher than that of the standard one, since the number of switches and devices such as fuses and switches is highest. The cost of this schedule can be high and this justifies the high initial investment inherent of fault-tolerant motor drive systems. The initial investment can be justified if the THD or losses of the conventional system is a critical factor. Parallel converter system permits to employ extra switches without increasing the final price of converter. In Brazil, it is quite common to have a single-phase distribution system and a demand to supply a three-phase motor in electric generating power station (WECS).

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